National Exams May 2018

04-Agric-B2

Structural Design of Agricultural, Biosystems and Food Industries 3 hours duration

NOTES:

- 1. If doubt exists as to the interpretation of any question, the candidate is urged to submit a clear statement of any assumptions made as part of the answer.
- 2. This is an OPEN BOOK EXAM.

 Any non-communicating calculator is permitted.
- 3. FIVE (5) questions constitute a complete exam paper.

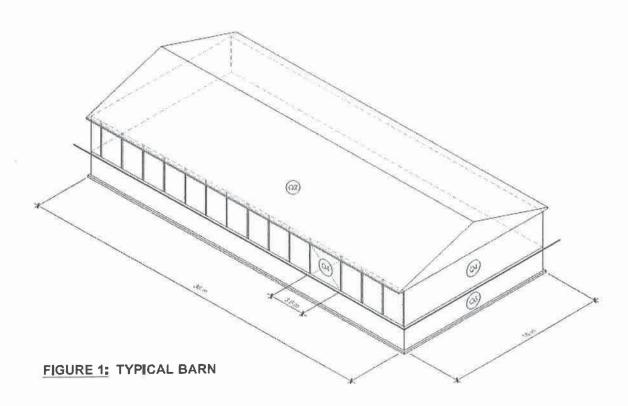
 Question 1 to be answered by all candidates plus 4 of the following 5 questions. The first five questions as they appear in the answer book will be marked.
- 4. Each question is of equal value.
- 5. Some questions require an answer in essay format. Clarity and organization of the answer is important. Provide sketches to illustrate the answer where applicable.

Question 1 (Mandatory question):

Define the following terms and explain their relationship to the structural design of agricultural structures; use examples to illustrate your answer. (20 marks, 4 marks each definition & explanation)

- a) Low Human Occupancy
- b) Limit States Design
- c) Lateral Force Resisting System
- d) Roof Slope factor
- e) Sulfate Resistant Concrete

The drawing below (Figure 1) is illustrative of a typical low human occupancy loose animal housing barn with below slab manure storage facility. This schematic drawing applies to questions 2 through 5.



Answer 4 of the following 5 questions:

Question 2:

- a) Determine the factored reactions at bearing locations 1 and 5 (5 marks)
- b) Determine the factored axial forces in members 1-2, 2-3, 2-8 and 7-8 for the truss illustrated in Figure 2 (15 marks).

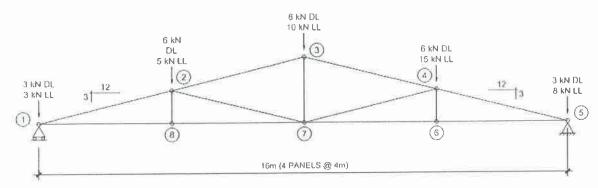


FIGURE 2: TRUSS ELEVATION

Question 3:

A lintel over a 4.8m wide side wall doors is to be made from built up (multi-ply) 38x286 [2x12] SPF No.1 members supported by 140x185 [6x8] SPF No. 1 wood posts. As illustrated below, the applied factored truss loads are applied at 1.2m on centre and it can be assumed that the truss load over a post is applied directly to the post.

- a) Using the attached CSA Standard O86-09 Table 6.3.1A for specified strength, design the required timber lintel B1. For the purpose of this design, the strength modification factors may be all taken as 1.0. (10 marks)
- b) Using the attached CSA Standard O86-09 Table 6.3.1D for specified strength, verify that the 140x185 timber post P1 is structurally adequate assuming that the stress ratio from wind induced bending is 44%. For the purpose of this design, the strength modification factor Kzc may be taken as 1.14 and Kc as 0.70. (10 marks)

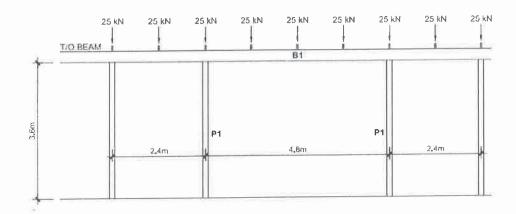


FIGURE 3: SIDE WALL BEAM / POST ELEVATIONS

Question 4:

- a) Based on the barn illustrated in Figure 1, discuss three lateral force resisting systems available to address wind forces. For each, describe the method for determining the magnitude of the lateral load to be resisted by system. (10 marks)
- b) Assuming that the wind lateral force resisting system is based on a diaphragm roof transferring the lateral load to the barn endwall, design and detail a diagonal wood brace system. For the purpose of this question, assume that a total factored wind lateral load of 25 KN is to be resisted at each end wall refer to Figure 4. (10 marks)

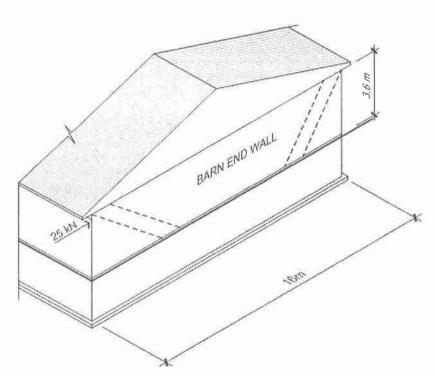


FIGURE 4: BARN END WALL ELEVATION

Question 5:

The below-floor rectangular concrete manure storage tank is 12m wide, 36m long and 2.4m deep. The exterior of the tank will be backfilled after construction. The tank is designed to safely store 240 days of liquid manure.

- a) Discuss the loads applied on the manure tank structure and the appropriate design considerations (10 marks)
- b) Manure storage is a very corrosive environment. Discuss the concrete design requirements including cement types, cement content, water/cement ratio, aggregates, admixtures, concrete cover, curing, and concrete cracking required to provide a durable storage facility. (10 marks)

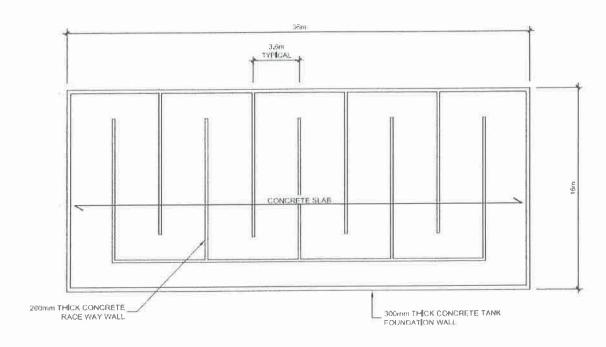


FIGURE 5: PLAN OF MANURE TANK

Question 6:

A horizontal or bunker silo is used for the storage of bulk animal feed such as whole-plant corn silage. The feed is placed and consolidated in the silo by tractor. The National Farm Building Code specifies the silage pressure at the wall as L=3.5 + 3.5H where L is the lateral load in kPa and H is the height of the wall in m. Design the reinforced concrete retaining walls required to resist the specified loads. Use 35 MPa concrete, 400 MPa reinforcing steel and a SLS soil bearing capacity of 150 kPa. (20 marks)

A)	Footing thickness:
B)	Footing heel length:
C)	Wall thickness:
D)	Footing toe length:
E)	Wall horizontal reinforcing steel:
Fί	Wall vertical reinforcing steel:

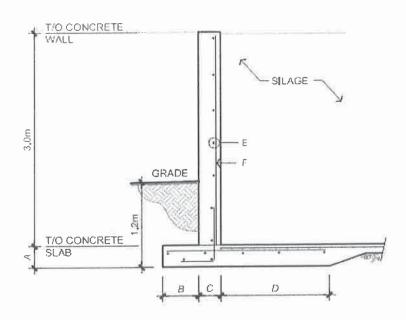


FIGURE 6: RETAINING WALL SECTION

Table 6.3.1A Specified strengths and modulus of elasticity for structural joist and plank, structural light framing, and stud grade categories of lumber, MPa

	Grade	Bending at extreme fibre, f _b	Longi- tudinal shear, f_v	Compression				
Species Identification				Parallel to grain,	Perpendicular to grain, f_{ip}	Tension parallel to grain, fi	Modulus of clasticity $E = E_{\mathrm{US}}$	
D Fir-L	SS	16.5		19.0		10.6	12 500	8 500
D Tile-95	No. 1/No. 2	10.0	1.9	14.0	7.0	5.8	11 000	7 000
	No. 3/Stud	4.6		7.3		2.1	10 000	5 500
Hem-Fir	55	16.0		17.6		9.7	12 000	8 500
110711111	No. 1/No. 2	11.0	1.6	14.8	4.6	6.2	11 000	7 500
	No. 3/Stud	7.0	1.7/5	9.2		3.2	10 000	6 000
Spruce-Pine-Fir	22	165		14.5		8.6	10 500	7 500
Sproce in the fit	No. 1/No.2	11.8	1.5	11.5	5.3	5.5	9 500	6 500
	No. 3/Stud	7.0		9.0		3.2	9 000	5 500
Northern	22	10.6		13.0		6.2	7 500	5 500
14076112111	No. 1/No. 2	7.6	1.3	10.4	3.5	4.0	7 000	5 000
	No. 3/Stud	4.5		5.2		2.0	6 500	4 000

Note: Tabulated values are based on the following standard conditions:

- (a) 286 mm larger dimension;
- (b) dry service conditions; and
- (c) standard-term duration of load.

Table 6.3.1D Specified strengths and modulus of elasticity for post and timber grades, MPa

	Grade	Bending at extreme fibre, f_b	Longi- tudinal shear, f _i	Compression		23		
Species identification				Parallel to grain,	Perpendicular to grain,	Tension parallel to grain, fe	$-\frac{\text{Modulus of elasticit}}{\mathbb{E}} \frac{E_{08}}{E_{08}}$	
D Fir-L	\$5	18.3	1.5	13.8	7.0	10.7	12 000	8 000
IJ TIIFE	No. 1	13.8		12.2		8.1	10 500	6 500
	No. 2	6.0		7.5		3.8	9 500	6 000
Hem-Fir	55	13.6	1.2	11.3	4.6	7.9	10 000	7 000
110,111	No. 1	10.2		10.0		6.0	9 000	6 000
	No. 2	4.5		6.1		2.8	8 000	5 500
Spruce-Pine-Fir	55	12.7	1.2	9,9	5.3	7.4	8 500	6 000
Springer in the Fin	No. 1	9.6		8.7		5.6	7 500	5 000
	No. 2	4.2		5,4		2.6	6 500	4 500
Northern	55	12.0	1.0	7.5	3.5	7.0	8 000	5 500
	No. 1	9.0		6.7		5.3	7 000	5 000
	No. 2	3.9		4.1		2.5	6 000	4 000

- (1) Posts and timbers have a smaller dimension of at least 114 mm, with a larger dimension not more than 51 mm greater than the smaller dimension.
- (2) Posts and timbers graded to beam and stringer rules may be assigned beam and stringer strength.
- (3) An approximate value for modulus of rigidity may be estimated at 0.065 times the modulus of elasticity.
 (4) With sown members thicker than 89 mm that season slowly, care should be exercised to availd overloading in compression before appreciable seasoning of the outer tibre has taken place; otherwise, compression strengths for wet
 - service conditions shall be used.
- (5) Tabulated values are based on the following standard canditions:
 - (a) 343 mm larger dimension for bending and shear and 292 mm larger dimension for tension and compression parallel to grain;
 - (b) dry service conditions; and
 - (c) standard-term duration of load.
- (6) The designer is strongly advised to check availability of species, grade, and sizes before specifying. See Clause A.G.2.J.2.

0.90

0.91

0.92

0.92

0.93

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Reinforcement ratio $|\rho|(\%)$ for rectangular sections with tension Table 2.1 rainforcement fy = 400 MPa

$$M_{s} = K_{s}bd^{2} \times 10^{-8} \text{ kN/m};$$
 $K_{s} = \frac{1}{1 - \frac{\rho \sigma I_{s}}{2\alpha_{s}\sigma_{s}f^{*}}} \frac{1}{\rho \sigma I_{s}} \frac{A_{s}}{bd}$

					0,00 []	35	β _i r <u>i</u>				
	h A,			2				= ⇒ 1			
		b						F.0	cc	60	
f'e (MPa)		20	25	30	35	40	45	50	55 0.77	0.76	
(1,		0.82	0.81	0.81	0.80	0,79	0.78	0.78	0.83	0.82	
Br B		0.92	0.91	0.90	88.0	0.87	0.88	0.85	4.27	4 55	
Pia s		1.83	2.24	2:63	3.00	3.34	3.67	3.98	421	4 00	
K,						(%)			0.16	0.15	
0.5		0.15	0.15	0.15	0.15	0.15	0,15	0.15	0.15		
0.6		0.18	0.18	0.18	0.18	0.18	0.18	6.18	0.18	0.18 0.21	
0.7		0.21	0.21	0.21	0.21	0.21	0.21	0.21	0.21		
0.8		0.24	0.24	0.24	0.24	0.24	0.24	0:24	0.24	0.24	
0.9		0.28	0.27	0.27	0.27	0,27	0.27	0.27	0.27	0.27	
			0.04	0.20	0.30	0.30	0.30	0.30	0.30	0.30	
1.0		0.31	0.31	0.30	0.33	0.33	0.33	0.33	0.33	0.33 -	
1.1		0.34	0.34	0.34	0.37	0.38	0.36	0.36	0.36	0,36	
1.2		0.38	0.37	0.37	0.40	0.40	0.39	0.39	0.39	0.39	
1.3		0.41	0.40	0.40	0.40	3.43	0.43	0.42	0.42	0.42	
1.4		0.44	0.44	0.43	0.40	0 40	0 10				
, ,=		0.48	0.47	0.46	0.46	0.46	0.46	0.46	0.45	0.45	
1.5		0.51	0.50	0.50	0.49	0.49	0.49	0.49	0.49	0.48	
1.6		0.55	0.54	0.53	0.53	0.52	0.52	0.52	0,52	0.52	
1.7			0.57	0.56	0.56	0.55	0.55	0.55	0.55	0.55	
1.8		0.58	0.61	0.60	0.59	0.59	0.58	0.58	0.58	0.58	
1.9		0.62	0.01	0.00	0,01					0.61	
2.0		0.66	0.64	0.63	0.62	0.62	0.62	0.61	0.61	0.64	
2.0		0.69	0.68	0.67	().66	0.65	0.65	0.65	0:64	0.67	
		0.73	0.71	0.70	0.69	0.69	0.68	0.68	0.68	0.70	
2.2		0.77	0.75	0.73	0.73	0.72	0.74	0.71	0.71	0.74	
2.3		0.17	0.79	0.77	0.76	0.75	0.75	0.74	0.74	U, (==	
2.4		17 0 1	27.					0.70	0.77	0.77	
2.5		0.85	0.82	0.81	0.79	0.79	0.78	0.78	0.80	0.80	
2.6		0.89	0.86	0.84	0.83	0.82	0.81	0.81	0.80	0.83	
2.7		0.93	0.90	0.88	0.86	0.85	0.85	0.84	0.87	0.87	
2.8		0.98	0.94	0.91	0.90	0.89	0.88	0.88	0.90	0.90	

0.95

1.02

2.8

2.9