## NATIONAL EXAMINATIONS

May 2013

## 04-BS-7 MECHANICS OF FLUIDS

Three (3) hours duration

## Notes to Candidates

1. This is a Closed Book examination.
2. Exam consists of two Sections. Section $A$ is Calculative ( 9 questions) and Section B is Analytical (4 questions).
3. Do seven (7) questions from Section A (Calculative) and three (3) questions from Section B (Analytical). Note that the Analytical Questions do not require detailed calculations but do require full explanations.
4. Ten (10) questions constitute a complete paper. (Total 50 marks).
5. All questions are of equal value. (Each 5 marks).
6. If doubt exists as to the interpretation of any question, the candidate is urged to submit, with the answer paper, a clear statement of any assumptions made.
7. Candidates may use one of the approved Casio or Sharp calculators.
8. Reference data for particular questions are given on pages 8 and 9. All pages of questions attempted are to be returned with the Answer Booklet showing where readings were taken and which data was used. Candidates must write their names on these pages.
9. Constants are given on page 10.
10. Reference Equations are given on pages 11 to 14.

## SECTION A CALCULATIVE QUESTIONS

Do seven of nine questions. Solutions to these questions must be set out logically with all intermediate answers and units given.

## QUESTION 1

Refer to the diagram below which shows a horizontal pipe to which a manometer is connected. The manometer has two openings to the atmosphere.

Determine the absolute pressure P in the pipe in kPa when the manometer readings are as shown in the diagram. Refer to the Constants on Page 10 for the specific gravities of the relevant fluids.

The pipe carries water and those manometer tubes which are open to atmosphere are subject to an atmospheric pressure head equal to 10 m of water.
(5marks)


## QUESTION 2

A hot air balloon as shown in the adjacent sketch is made in the shape of a sphere with a cone at the bottom. The diameter of the sphere is 18 m and the side of the cone is at an angle of $45^{\circ}$ to the vertical axis. This gives the balloon a total volume of $3147 \mathrm{~m}^{3}$. The total mass is made up as follows:

| Envelope | 100 kg |
| :--- | ---: |
| Basket | 60 kg |
| Fuel Tanks | 110 kg |
| Burners | 50 kg |
| Two People | 160 kg |



Determine the temperature of the hot air inside the balloon envelope to establish neutral buoyancy (equilibrium) in the atmosphere. The ambient atmospheric conditions are 100 kPa and $15^{\circ} \mathrm{C}$.
( 5 marks)

## QUESTION 3

Refer to the illustration alongside. The angle of the gate is $90^{\circ}$ as shown, the mass of the gate is 400 kg , the horizontal width of the gate 1.0 m , the length of the small arm 1.2 m , and the centre of gravity 0.3 m to right of and 0.3 m above pivot O . Neglect friction at the pivot and thickness of the gate. If the depth of water $x$ above the pivot is 2 m , state whether the gate will open or remain closed.

(5 marks)

## QUESTION 4

Water flows at a rate of 0.300 L s through a small circular hole in the bottom of a large tank. Assuming the water in the tank approaches the hole radially, calculate the velocity in the tank at a distance of 100 mm from the hole.

( 5 marks)

## QUESTION 5

For ideal flow (no friction) the velocity $V_{1}$ around the surface of a long cylinder is given by $V_{1}=2 V_{0} \sin \theta$ where $V_{0}$ is the free stream velocity and $\theta$ the angular location around the cylinder measured from the front (stagnation point). Consider a concrete chimney 20 m in diameter and 275 m in height subject to a wind velocity of 100 $\mathrm{km} / \mathrm{hr}$. Determine the velocity and pressure of the air on the front (stagnation point point 1) and sides ( $90^{\circ}$ from stagnation point - point 2) of the chimney. Express the pressure relative to atmospheric pressure (gauge pressure).

## QUESTION 6

Preformed fibre insulation panels 2.438 m $\times 1.219 \mathrm{~m} \times 25 \mathrm{~mm}$ are used to insulate a building. During construction some are left lying flat on grass as shown in the adjoining sketch. If the density of a panel is $100 \mathrm{~kg} / \mathrm{m}^{3}$ calculate the minimum wind velocity (in $\mathrm{km} / \mathrm{hr}$ ) at ground level which will lift the panel and blow it away. Note that the grass under the panel reduces the air velocity to stagnation conditions.

( 5 marks)

(5 marks)

## QUESTION 7

A propeller of 2 m in diameter is mounted on an aircraft travelling at $500 \mathrm{~km} / \mathrm{hr}$. The airstream leaves the propeller with a velocity of $650 \mathrm{~km} / \mathrm{hr}$. Assume that the pressure upstream and downstream of the propeller is equal to atmospheric pressure and that the flow converges as the velocity increases. Determine the thrust developed by the propeller.

( 5 marks)

## QUESTION 8

## Refer to the Examination Paper Attachments Page 8 Moody Diagram

A 2.0 m diameter concrete pipe of length 1560 m , for which the roughness is 1.5 mm , conveys water between two reservoirs at a rate of $8.0 \mathrm{~m}^{3} / \mathrm{s}$. Determine the required difference in water surface elevation between the two reservoirs. Use the attached Moody diagram to obtain the friction factor.

Return the diagram with your answer booklet to show your readings.
( 5 marks)

## QUESTION 9

Refer to the Examination Paper Attachments Page 9 Drag Coefficient Diagram
A meteorological balloon filled with hydrogen may be used for tracking wind directions in the atmosphere. If such a balloon is 600 mm in diameter when filled and has negligible mass determine its rate of rise through the lower atmosphere. Assume that the internal pressure is the same as that of the atmosphere and that it is spherical in shape. Assume constant diameter and constant densities while in the lower atmosphere. Obtain the answer by plotting on the attached Drag Coefficient Diagram and drawing a line through the plotted point.

Return the diagram with your answer booklet to show your working.
Hint: Set up equations of $C_{D}$ and Re in terms of balloon velocity $V$ and plot points for various guessed values of $V$ on the chart.

## DESCRIPTIVE QUESTIONS

## Do three of four questions. These questions do not require detailed calculations but complete written explanations must be given to support the answers.

## QUESTION 10



Two ponds contain light oil and quicksand (a slurry of fine sand and water in suspension) as shown above. State in which humans are more likely to sink. Give a full explanation for your answer.

$$
\text { ( } 5 \text { marks ) }
$$

## QUESTION 11



DAM A


DAM B

Two small L-shaped dams are built on a firm flat surface as shown above. Assuming that there is no seepage under the wall but that sliding can occur, state which dam Dam A or Dam B - will be most likely to slide. Explain fully why one will be more likely to slide than the other.

## QUESTION 12



A barge 15 m long and 3 m wide is loaded such that its draught (depth of bottom below water surface) is 1.2 m . It sails in a long canal 5 m wide and 2 m deep. At one point the canal is taken across a valley by an aqueduct as shown in the sketch above. Determine the change in compressive force on the aqueduct pillars as the barge passes over them. Give a full explanation of your answer.
(5 marks)

## QUESTION 13



Pointed Prolate Spherical


Oblate (Flattened)

With reference to the sketches above state what shape a very large rain drop falling through the atmosphere is likely to assume - prolate, spherical or oblate. Explain fully why it would assume the chosen shape and compare this shape with the likely shape of a very smali raindrop.

EXAMINATION PAPER ATTACHMENTS 04-BS-7 May 2013 Page 8 of 14 QUESTION 8 MOODY DIAGRAM

NAME $\qquad$
Values of ( $D V$ ) for water at $15^{\circ} \mathrm{C}$ (diameter in mm $\times$ velocity in $\mathrm{m} / \mathrm{s}$ )

Moody chart for pipe friction factor (Stanton diagram).

NAME $\qquad$

31210 Forces on Immersed Bodies

Figure 10.10 Drag coefficient for bodies of revolution. (Adapted from L. PrandtL, "Ergebaisse der aerodynamischen Versuchsanstalt zu Göttingen," p. 29, R. Oldenbourg, Munich and Berlin, 1923; and F. Eisper, "Das Widerstandsproblem," Proc. $3 d$ Internatn. Congr. Appl. Mech.,

## 04-BS-7 MECHANICS OF FLUIDS

## GENERAL REFERENCE INFORMATION

## CONSTANTS

In engineering calculations a high degree of accuracy is seldom attained due to the neglect of minor influences or the inaccuracy of available data. For consistency in calculations however the following reasonably accurate constants should be used:

Atmospheric Pressure $\mathrm{p}_{\mathrm{o}}=100 \mathrm{kPa}$
Gravitational Acceleration $\mathrm{g}=9.81 \mathrm{~m} / \mathrm{s}^{2}$
Specific Gravity of Water $=1.00$
Specific Gravity of Glycerine $=1.26$
Specific Gravity of Mercury $=13.56$
Specific Gravity of Benzene $=0.90$
Specific Gravity of Carbon Tetrachloride $=1.59$
Density of Water $\rho=1000 \mathrm{~kg} / \mathrm{m}^{3}$
Density of Sea Water $\rho=1025 \mathrm{~kg} / \mathrm{m}^{3}$
Density of Concrete $p=2400 \mathrm{~kg} / \mathrm{m}^{3}$
Density of Air $\rho=1.19 \mathrm{~kg} / \mathrm{m}^{3}$ (at $20^{\circ} \mathrm{C}$ ), $\rho=1.21 \mathrm{~kg} / \mathrm{m}^{3}$ (at $15^{\circ} \mathrm{C}$ )
Absolute Viscosity of Water $\mu=1.0 \times 10^{-3} \mathrm{Ns} / \mathrm{m}^{2}$
Absolute Viscosity of Air $\mu=1.8 \times 10^{-5} \mathrm{Ns} / \mathrm{m}^{2}$
Surface Tension of Water $\sigma=0.0728 \mathrm{~N} / \mathrm{m}$ (at $20^{\circ} \mathrm{C}$ )
Specific Heat of Water $c_{p}=4.19 \mathrm{~kJ} / \mathrm{kg}^{\circ} \mathrm{C}$
Specific Heat of Air $c_{p}=1005 \mathrm{~J} / \mathrm{kg}^{\circ} \mathrm{C}$
Specific Heat of Air $\mathrm{C}_{\mathrm{p}}=718 \mathrm{~J} / \mathrm{kg}{ }^{\circ} \mathrm{C}$
Gas Constant for Air R $=287 \mathrm{~J} / \mathrm{kg}^{\circ} \mathrm{K}$
Gas Constant for Helium R $=2077 \mathrm{~J} / \mathrm{kg}{ }^{\circ} \mathrm{K}$
Gas Constant for Hydrogen $\mathrm{R}=4120 \mathrm{~J} / \mathrm{kg}^{\circ} \mathrm{K}$

## NOMENCLATURE FOR REFERENCE EQUATIONS (SI UNITS)

| a | Width | m |
| :---: | :---: | :---: |
| A | Flow area, Surface area | $\mathrm{m}^{2}$ |
| CV | Calorific value | J/kg |
| $c_{p}$ | Specific heat at constant pressure | $\mathrm{J} / \mathrm{kg}^{\circ} \mathrm{C}$ |
| b | Width | m |
| D | Diameter | m |
| E | Energy | J |
| F | Force | N |
| 9 | Gravitational acceleration | $\mathrm{m} / \mathrm{s}^{2}$ |
| h | System head | m |
| $h_{L}$ | Head loss | m |
| H | Pump or turbine head | m |
| 1 | Moment of inertia | $\mathrm{m}^{4}$ |
| k | Ratio of specific heats |  |
| k | Loss coefficient |  |
| K | Constant |  |
| L | Length | m |
| m | Mass | kg |
| M | Mass flow rate | kg/s |
| N | Rotational speed | $\mathrm{rev} / \mathrm{s}$ |
| p | Pressure | $\mathrm{Pa}\left(\mathrm{N} / \mathrm{m}^{2}\right)$ |
| P | Power | W ( $\mathrm{J} / \mathrm{s}$ ) |
| q | Specific heat | J/kg |
| Q | Flow rate | $\mathrm{m}^{3} / \mathrm{s}$ |
| r | Radius | m |
| R | Specific gas constant | J/kg K |
| T | Temperature | K |
| U | Blade velocity | $\mathrm{m} / \mathrm{s}$ |
| $v$ | Specific volume | $\mathrm{m}^{3} / \mathrm{kg}$ |
| V | Velocity | $\mathrm{m} / \mathrm{s}$ |
| V | Volume | $\mathrm{m}^{3}$ |
| w | Specific work | $\mathrm{J} / \mathrm{kg}$ |
| W | Work | J |
| y | Depth | m |
| $z$ | Elevation | m |
| 7 | Efficiency |  |
| $\mu$ | Dynamic viscosity | $\mathrm{Ns} / \mathrm{m}^{2}$ |
| v | Kinematic viscosity | $\mathrm{m}^{2} / \mathrm{s}$ |
| $\rho$ | Density | $\mathrm{kg} / \mathrm{m}^{3}$ |
| 0 | Surface tension | N/m |
| T | Thrust |  |
| T | Shear stress | $\mathrm{N} / \mathrm{m}^{2}$ |

## REFERENCE EQUATIONS

Equation of State

$$
\begin{aligned}
& p v=R T \\
& p=\rho R T
\end{aligned}
$$

## Universal Gas Law

$$
\rho v^{n}=\text { constant }
$$

Compressibility

$$
\beta=-\Delta / V \Delta p
$$

Viscous Force and Viscosity

$$
\begin{aligned}
& F=\mu A d u / d y \\
& \mu=\tau d u / d y \\
& v=\mu / \rho
\end{aligned}
$$

Capillary Rise and Internal Pressure due to Surface Tension

$$
\begin{aligned}
& \mathrm{h}=(\sigma \cos \theta / \rho \mathrm{g}) \times(\text { perimeter } / \text { area }) \\
& \mathrm{p}
\end{aligned}
$$

## Pressure at a Point

$$
p=\rho g h
$$

## Forces on Plane Areas and Centre of Pressure

$$
\begin{aligned}
& \mathrm{F}=\rho \rho y_{c} A \\
& y_{p}=y_{c}+I_{c} / y_{c} A
\end{aligned}
$$

Moments of Inertia
Rectangle: $\mathrm{I}_{\mathrm{c}}=\mathrm{bh}^{3} / 12$
Triangle: $\quad \mathrm{I}_{\mathrm{c}}=\mathrm{bh}^{3} / 36$
Circle: $\quad I_{c}=\pi D^{4} / 64$

Volumes of Solids

```
Sphere: \(\quad V=\pi D^{3} / 6\)
Cone: \(\quad V=\pi D^{2} h / 12\)
Spherical Segment: \(V=\left(3 a^{2}+3 b^{2}+4 h^{2}\right) \pi h / 2 g\)
```

Continuity Equation

$$
\rho_{1} V_{1} A_{1}=\rho_{2} V_{2} A_{2}=M
$$

## General Energy Equation

$$
\begin{aligned}
& p_{1} / \rho_{1} g+z_{1}+v_{1}{ }^{2} / 2 g+q_{\text {in }} / g+w_{\text {in }} / g \\
& =p_{2} / \rho_{2} g+z_{2}+V_{2}^{2} / 2 g+h_{L}+q_{\text {out }} / g+w_{\text {out }} / g
\end{aligned}
$$

Bernoulli Equation

$$
p_{1} / \rho g+z_{1}+V_{1}^{2} / 2 g=p_{2} / \rho g+z_{2}+V_{2}^{2} / 2 g
$$

Momentum Equation
Conduit: $\quad F_{R}=p_{1} A-p_{2} A-M\left(V_{2}-V_{1}\right)$
Free Jet: $\quad F_{R}=-\rho Q\left(V_{2}-V_{1}\right)$
Flow Measurement

| Venturi Tube: | $\mathrm{Q}=\left[\mathrm{CA}_{2} /\left\{1-\left(\mathrm{D}_{2} / \mathrm{D}_{1}\right)^{4}\right\}^{1 / 2}\right][2 \mathrm{~g} \Delta \mathrm{~h}]^{1 / 2}$ |
| :--- | :--- |
| Flow Nozzle: | $\mathrm{Q}=\mathrm{KA}_{2}[2 \mathrm{~g} \Delta \mathrm{~h}]^{1 / 2}$ |
| Orifice Meter: | $\mathrm{Q}=\mathrm{KA}_{0}[2 \mathrm{~g} \Delta \mathrm{~h}]^{1 / 2}$ |

## Flow over Weirs

Rectangular Weir: $\mathrm{Q}=\mathrm{C}_{\mathrm{d}}(2 / 3)[2 \mathrm{~g}]^{1 / 2} \mathrm{LH}^{3 / 2}$
Power
Turbomachine: $\quad P=\rho g Q H$
Free Jet: $\quad P=1 / 2 \rho Q V^{2}$

Moving Blades: $\quad P=M \Delta V U$

## Aircraft Propulsion

$$
\begin{aligned}
F_{\text {thrust }} & =M\left(V_{\text {jet }}-V_{\text {aiccraft }}\right) \\
P_{\text {thrust }} & =M\left(V_{\text {let }}-V_{\text {alicraft }}\right) V_{\text {aircraft }} \\
E_{\text {jet }} & =1 / 2\left(V_{\text {jet }}-V_{\text {gircraft }}{ }^{2}\right) \\
P_{\text {jet }} & =1 / 2 M\left(V_{\text {iet }}{ }^{2}-V_{\text {aircraftit }}{ }^{2}\right)
\end{aligned}
$$

$$
\begin{aligned}
& E_{\text {fuel }}=C V_{\text {fuel }} \\
& P_{\text {fuel }}=M_{\text {fuel }} C V_{\text {fuel }} \\
& \eta_{\text {thermal }}=P_{\text {iel }} / P_{\text {fuel }} \\
& \eta_{\text {propulsion }}=P_{\text {thrust }} / P_{\text {jet }}=2 V_{\text {aircrah }} /\left(V_{\text {jet }}+V_{\text {aircratt }}\right) \\
& \eta_{\text {overall }}=\eta_{\text {thermal }} \times \eta_{\text {propuision }}
\end{aligned}
$$

Wind Power

$$
\begin{aligned}
& P_{\text {total }}=1 / 2 \rho A_{T} V_{1}{ }^{3} \\
& P_{\text {max }}=8 / 27 \rho A_{T} V_{1}^{3} \\
& H_{\text {max }}=P_{\text {max }} / P_{\text {total }}=16 / 27
\end{aligned}
$$

Reynolds Number

$$
R e=d V \rho / \mu
$$

Flow in Pipes
$h_{L}=f(L / D)\left(V^{2} / 2 g\right)$
$\mathrm{D}_{\mathrm{e}}=4$ (flow area) $/$ (wetted perimeter)
$D=D_{e}$ for non-circular pipes
$L=L_{\text {total }}+L_{e}$ for non-linear pipes
$(L / D)=35 k \quad$ for $R e \sim 10^{4}$
Drag on Immersed Bodies
Friction Drag: $\quad F_{f}=C_{f} 1 / 2 \rho V^{2} B L \quad(B=\pi D)$
Pressure Drag: $\quad F_{p}=C_{p} 1 / 2 \rho V^{2} A$
Total Drag:
$F_{D}=C_{D} 1 / 2 \rho V^{2} A$
$\begin{array}{ll}\text { Aircraft Wing: } & F_{L}=C_{L} 1 / 2 \rho V^{2} A_{\text {wing }} \\ \text { Aircraft Wing: } & F_{D}=C_{D} 1 / 2 \rho V^{2} A_{\text {wing }}\end{array}$
Karmen Vortex Frequency

$$
f \approx 0.20(V / D)(1-20 / R e)
$$

